



Data Reduction and Its Impact on Test-Analysis Correlation

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Presentation Outline



- **Overview**
- **Background**
- **Predicted and Measured Results**
- **Concluding remarks**



Overview



Objective: Evaluate data analysis/signal processing technologies for crash applications to better quantify the accuracy of simulation results

Motivation:

- Document modeling improvements
- Evaluate design configurations analytically
- Enable analysis to further aid certification process

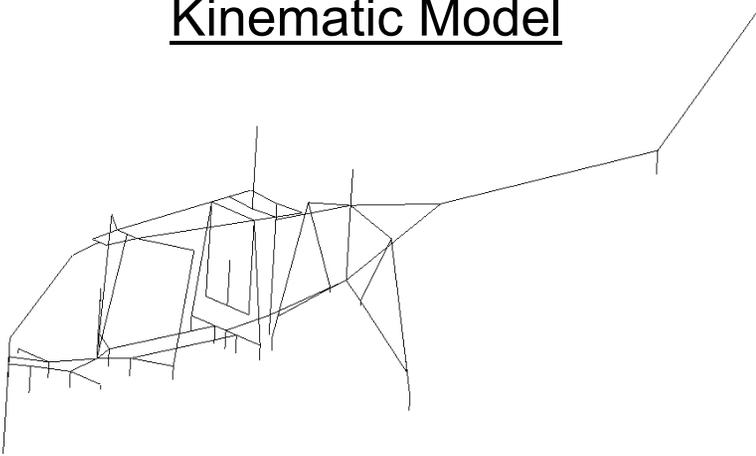
Current Project Thrusts:

- Simple metallic beam and plate structures
- Representative advanced-concept, composite fuselage section



Background

Kinematic Model

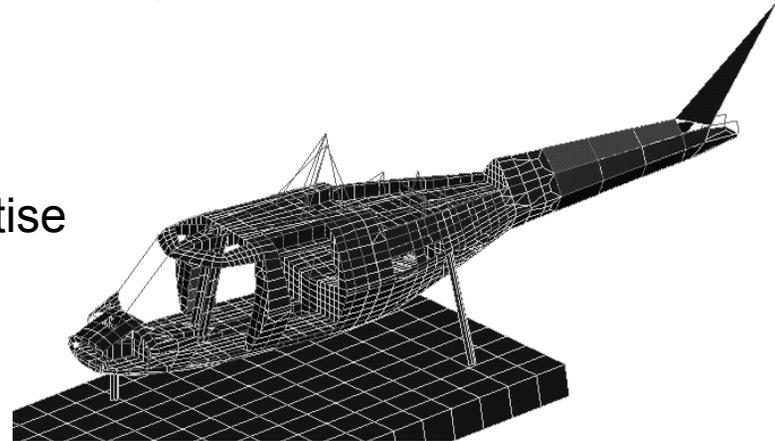


- Less than 100 nodes
- Concentrated masses, beams and 'crush' springs (based on empirical information)
- Requires numerous approximations and significant engineering judgment
- Calculates structural loading
- Computationally inexpensive



Nonlinear Dynamic Finite Element Model

- 4,000-400,000 nodes
- Shell, beam, solid elements and concentrated masses
- Requires significant analytical expertise
- Calculates structural behavior
- Computationally expensive

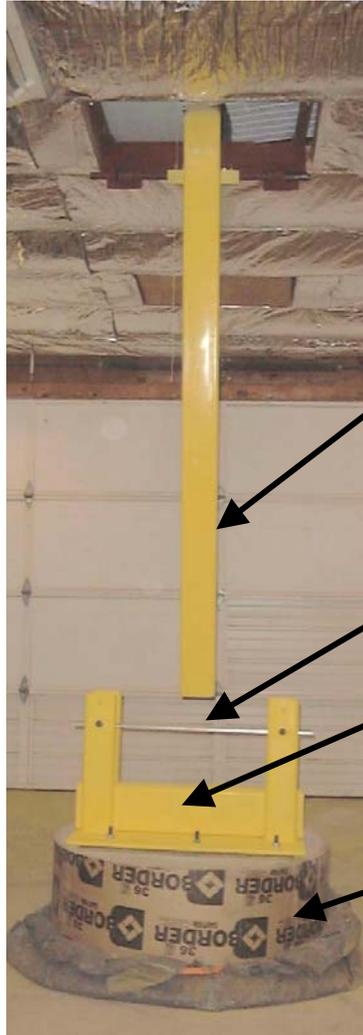


Need efficient methods to reduce, evaluate, and correlate large amounts of data



Metallic Beam and Plate Tests

Objective: Evaluate test and analysis correlation methods on simple structures with “known” responses



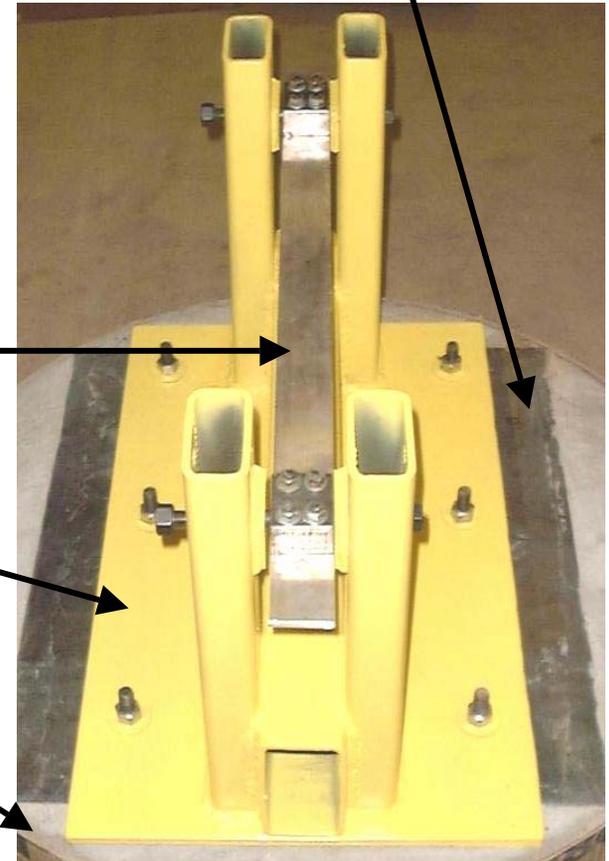
Semi-cylindrical impactor:
4 x 4 in. cross-section
24 in. long
16 lb. weight

Test beam

Test fixture

36-in diameter
concrete mounting
base - 1400 lb.

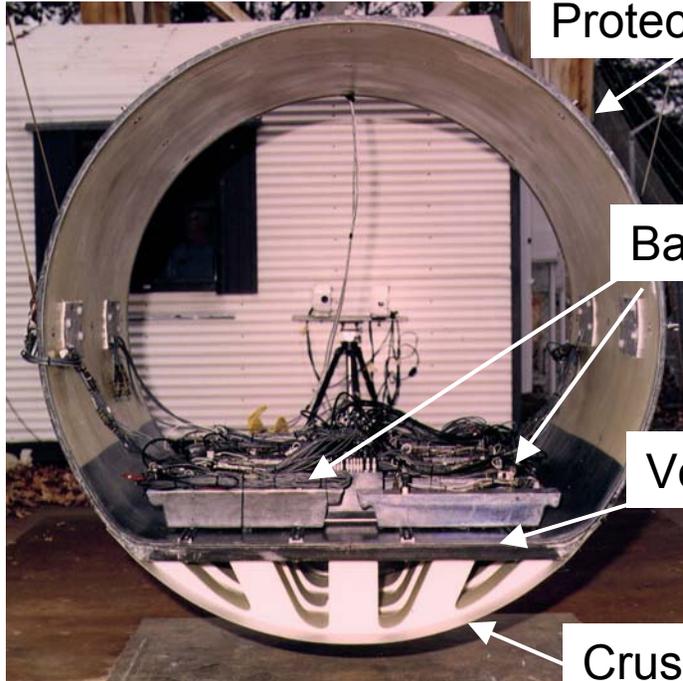
Imbedded steel
plate provides flat
mounting surface





Fuselage Section Description

Pre-test Photograph



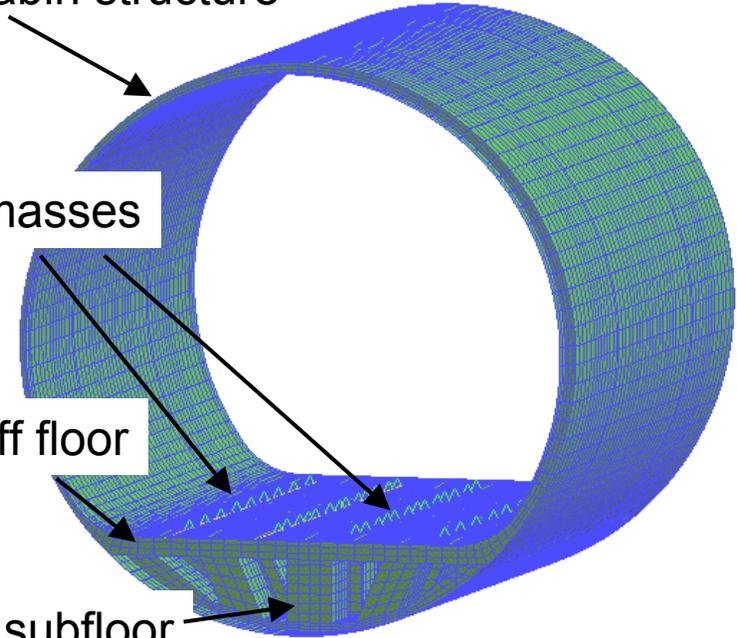
Finite Element Model

Protective cabin structure

Ballast masses

Very stiff floor

Crushable subfloor



- Dimensions: 60-in. diameter x 64-in. long
- Protective cabin: Foam with laminated composite face sheets
- Ballast: Ten 100-lb. lead weights
- Stiff floor: Provides global crushing of subfloor
- Subfloor: Foam with uniform crush properties

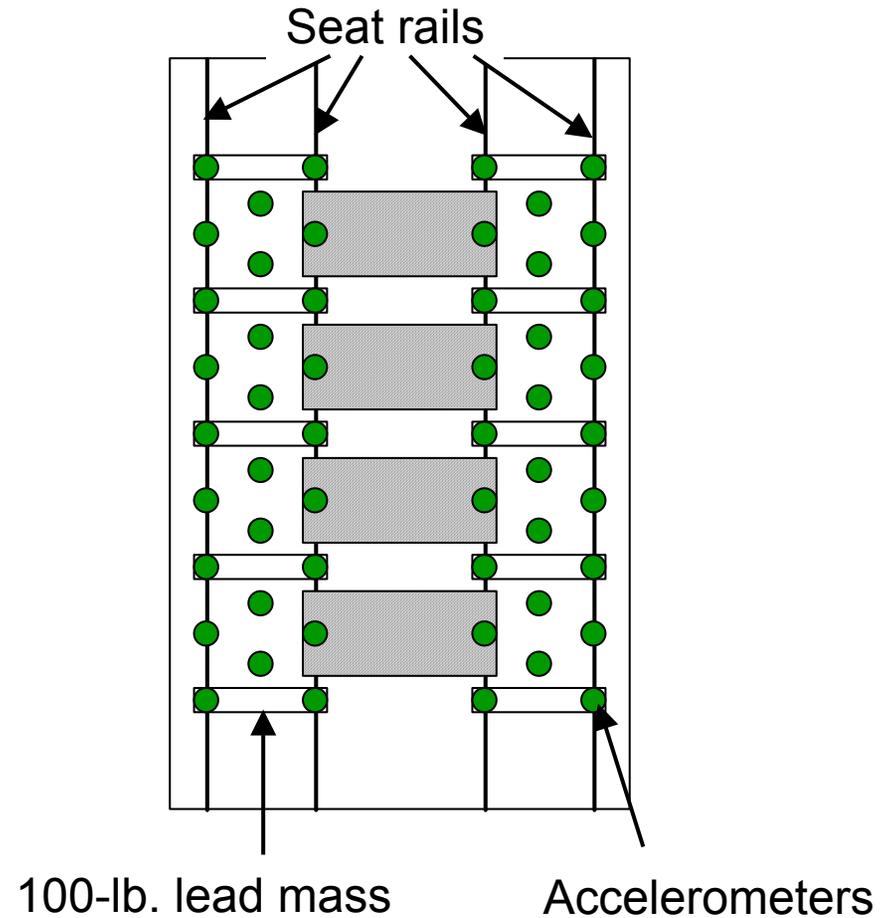


Section Test Summary

Test Conditions

- *Designed for correlation with FEM, NOT concept evaluation*
- Impact velocity 307 in/sec
- No roll, pitch or yaw
- 16-bit digital DAS
- 10 kHz sampling rate
- 73 accelerometers

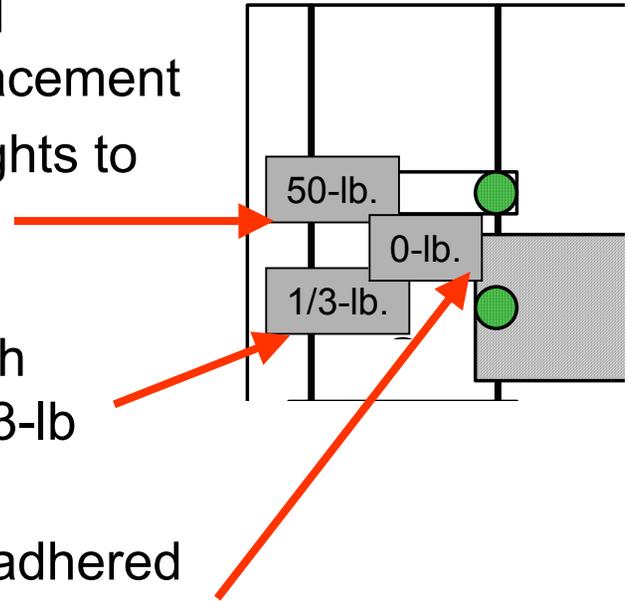
Floor Instrumentation





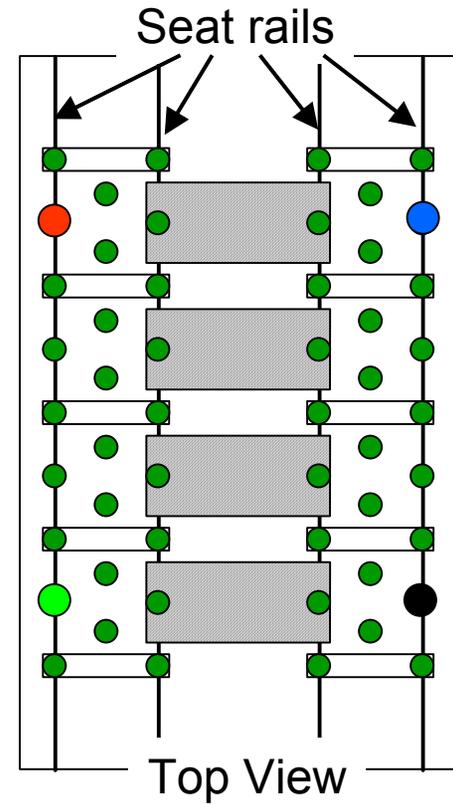
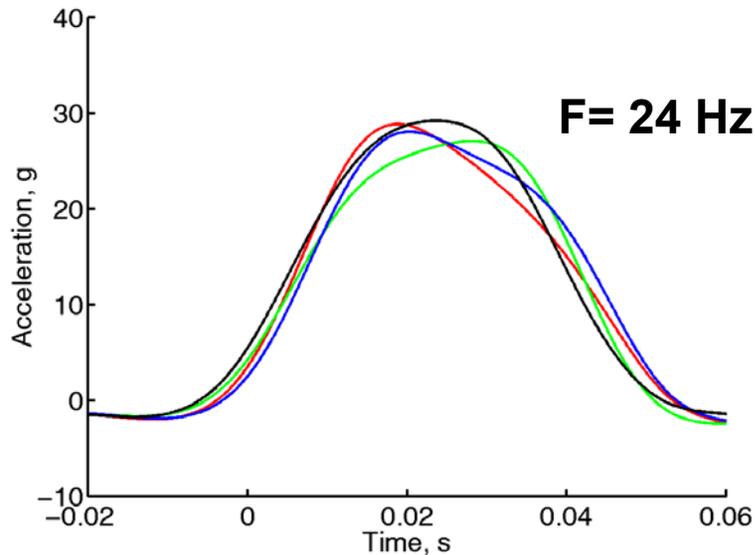
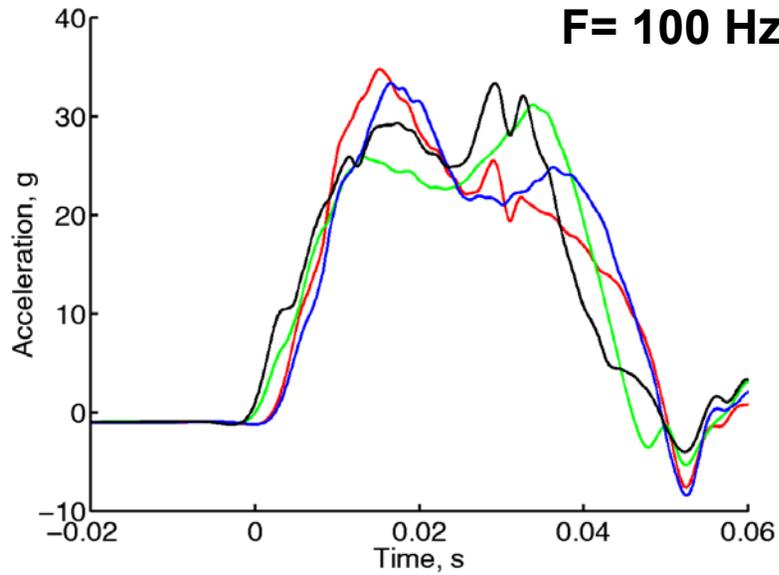
Instrumentation Details

- Densely instrumented structure enabled evaluation of effect of accelerometer placement
 - Location A - attachment of lead weights to seat rails, approximated as 50-lb concentrated mass on node.
 - Location B - Attached to seat rail with mounting block, approximated as 1/3-lb concentrated mass on node.
 - Location C - Mounted on block and adhered directly to floor, no concentrated mass at node.
- Known:
 - Global motion of stiff floor similar at all locations.





Sample Test Data (Symmetric locations)

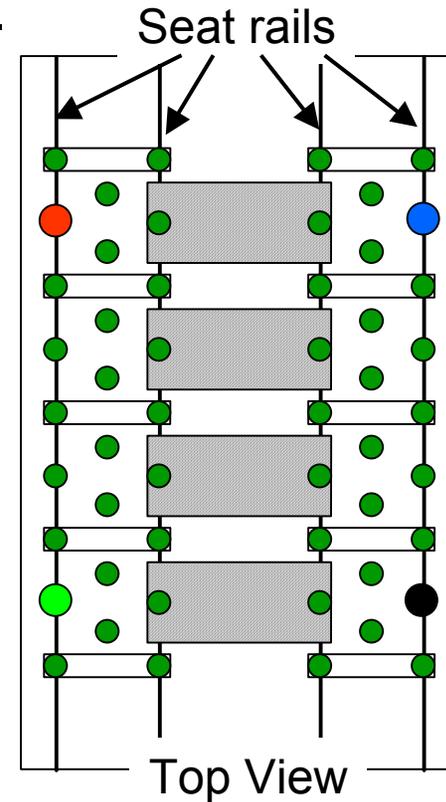
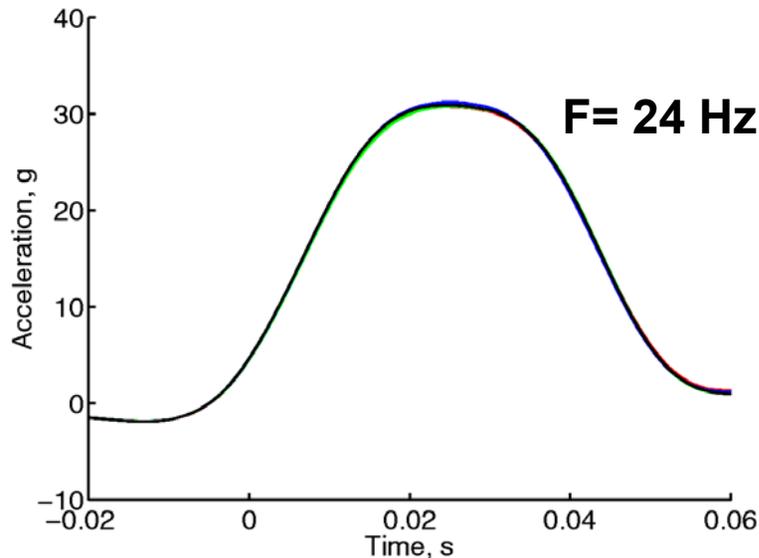
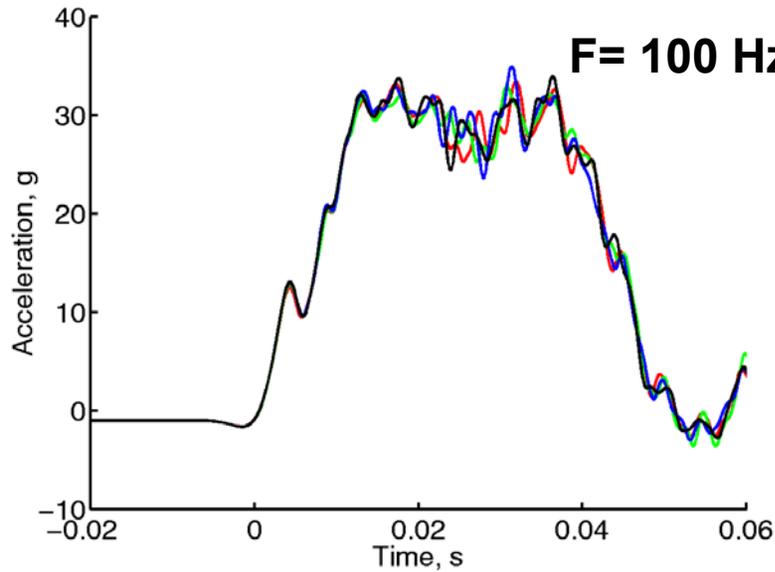


Filtering Frequency, Hz	Variation	
	Maximum	Mean
100	3.6	0.8
24	1.1	0.7



Sample Predicted Results

(Symmetric locations)

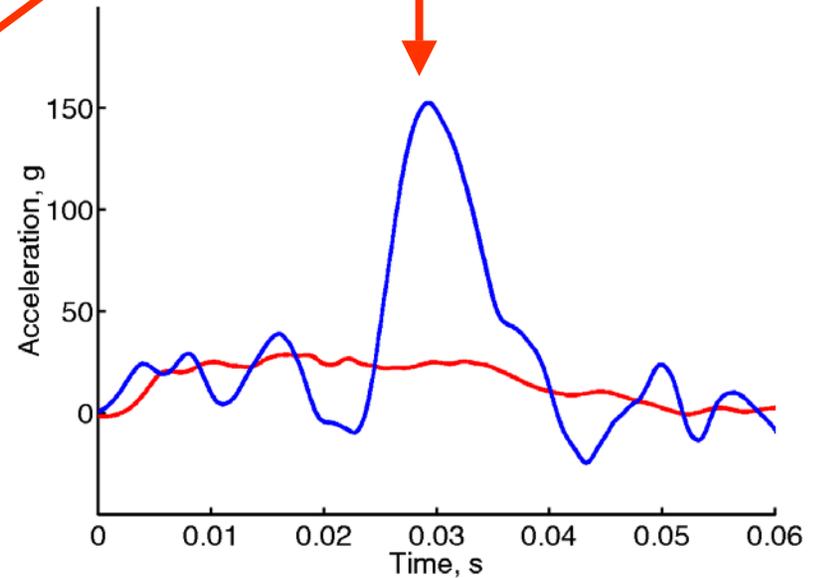
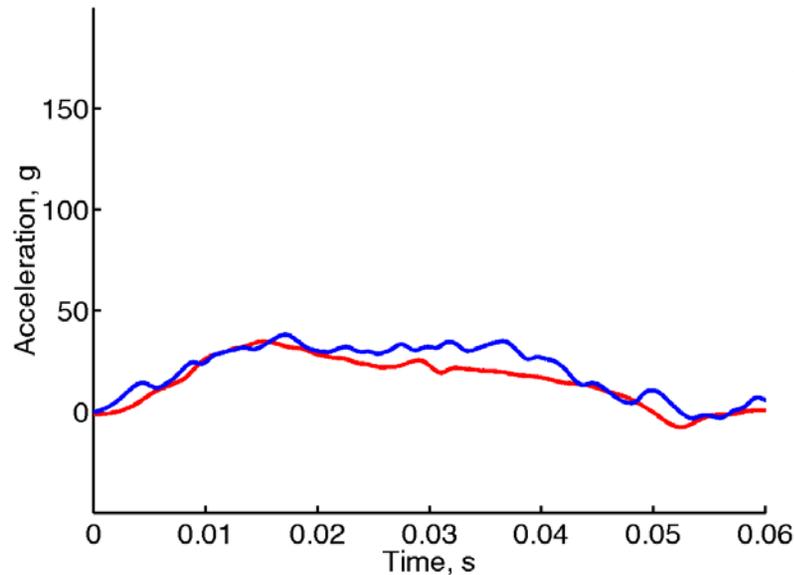
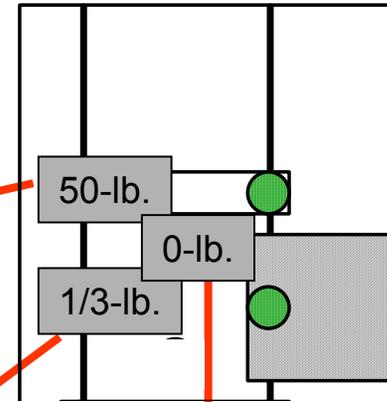
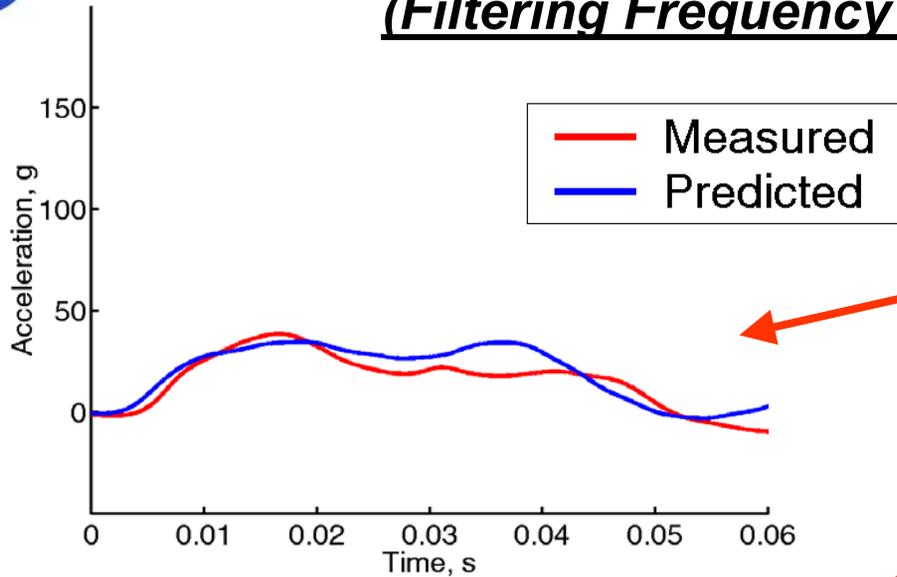


Filtering Frequency, Hz	Variation	
	Maximum	Mean
100	2.0	< 0.1
24	0.3	< 0.1



Correlation of Test Data and Predictions

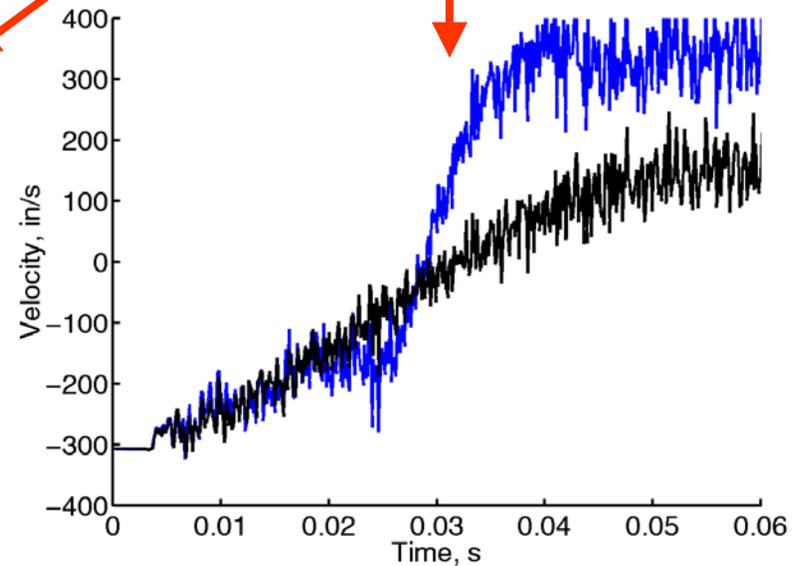
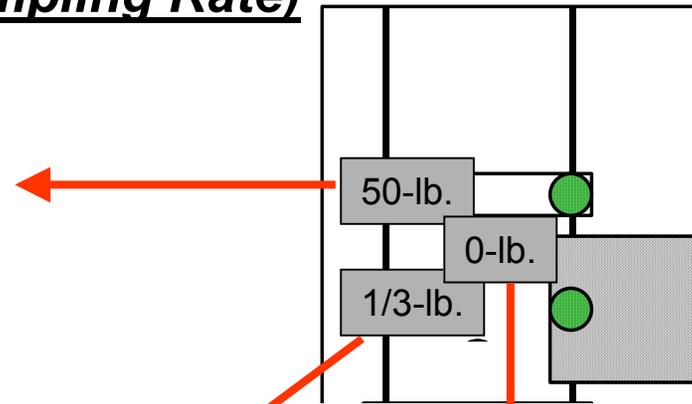
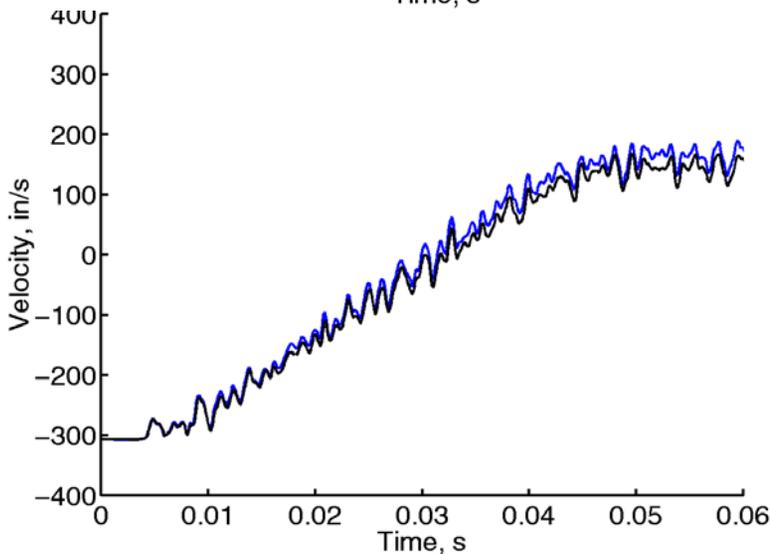
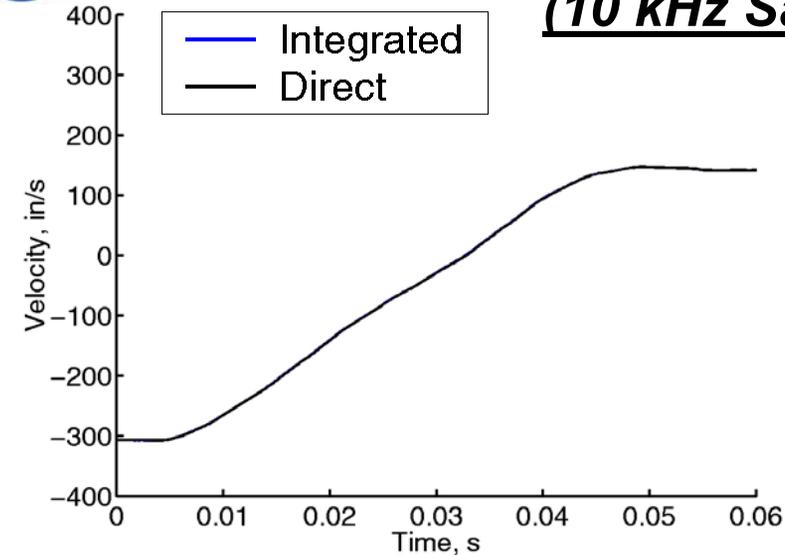
(Filtering Frequency = 100 Hz)



Why the discrepancy when no mass added to node?



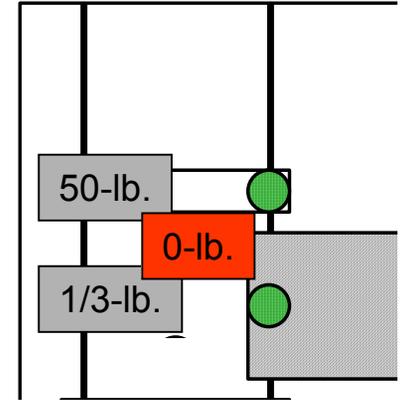
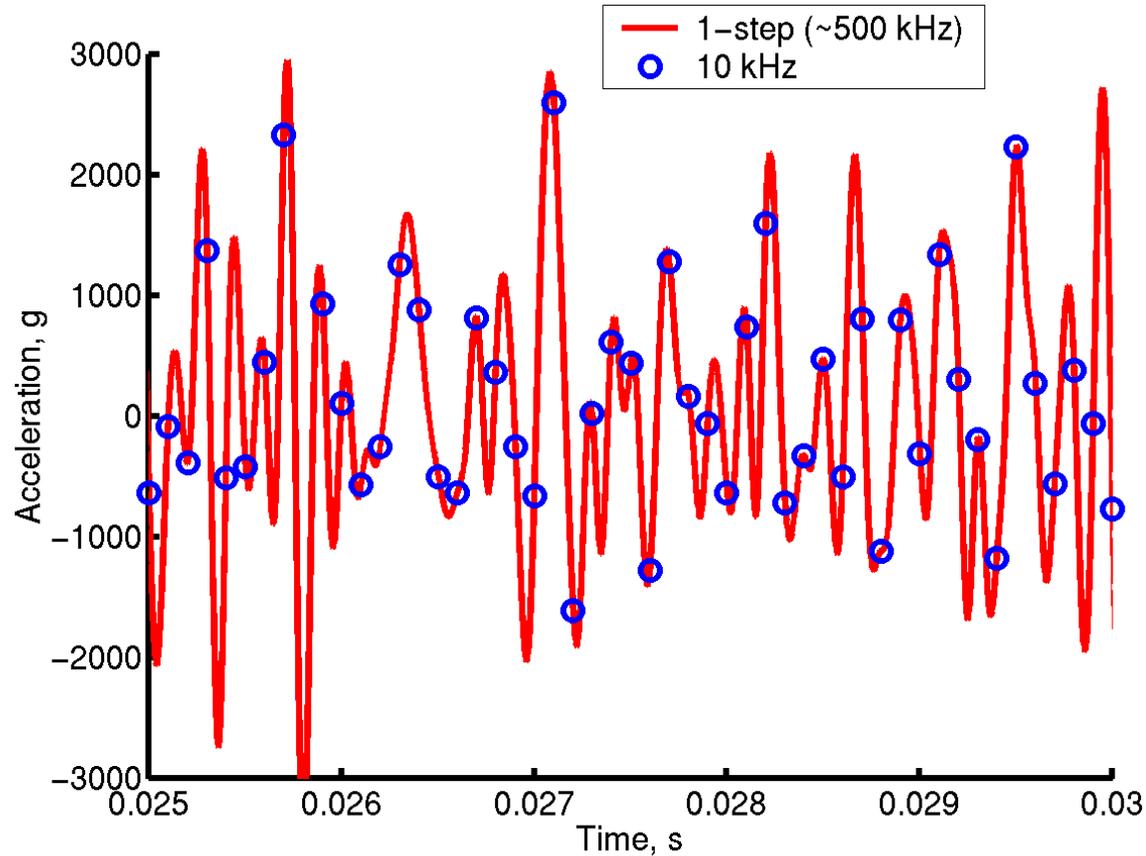
Predicted Velocities (10 kHz Sampling Rate)



“Integrated” velocities consistent with filtered accelerations,
but not consistent with “Direct” velocities



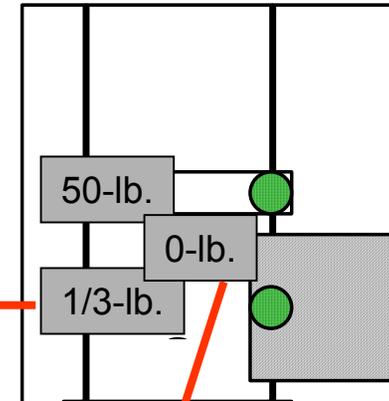
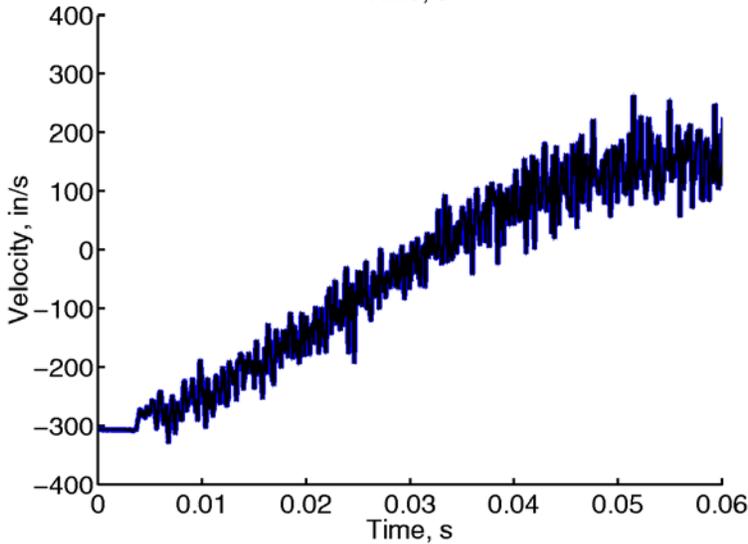
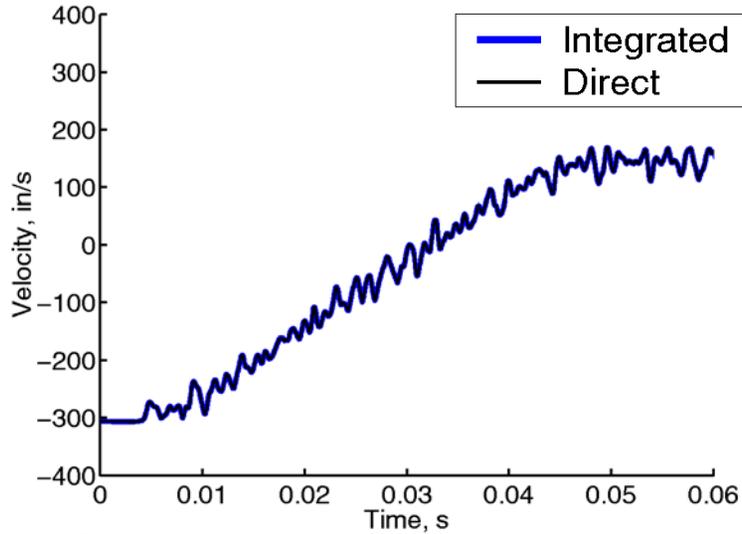
Sample Time History



Predicted accelerations repeatable from “run” to “run”



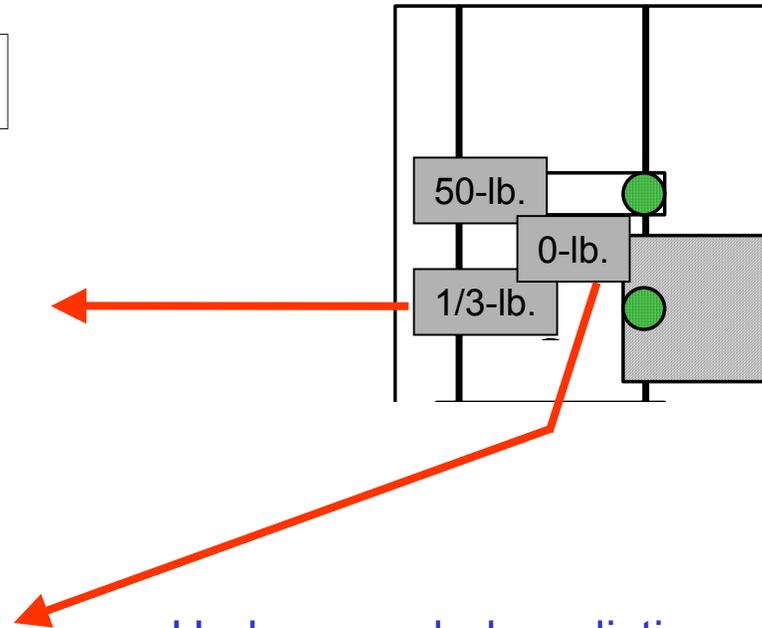
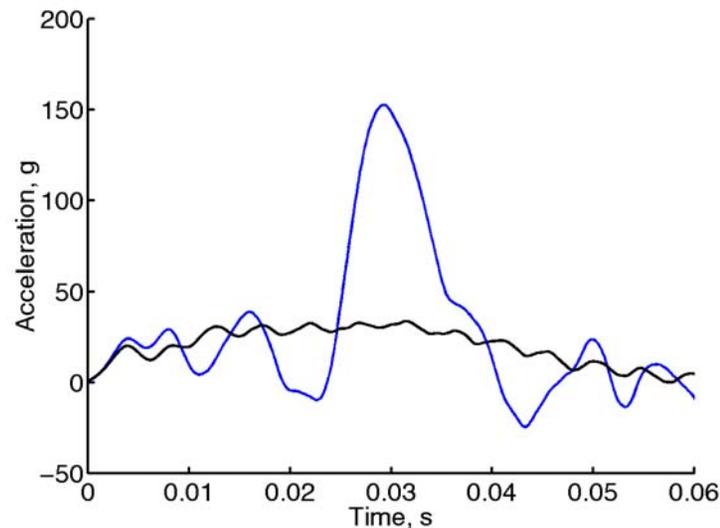
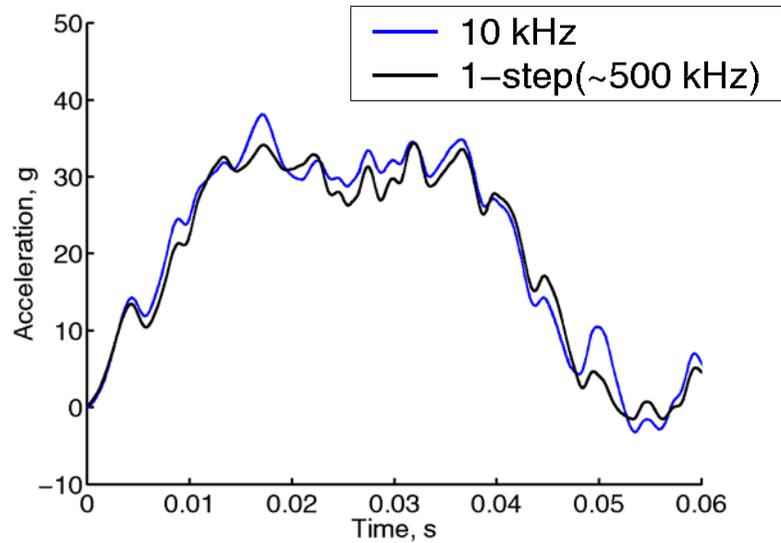
Predicted Velocities (1-step Sampling Rate)



No discrepancy between
“Integrated” and “Direct” velocity
values for data sampled every time
step.



Effect of Sampling Rate on Filtered Accelerations



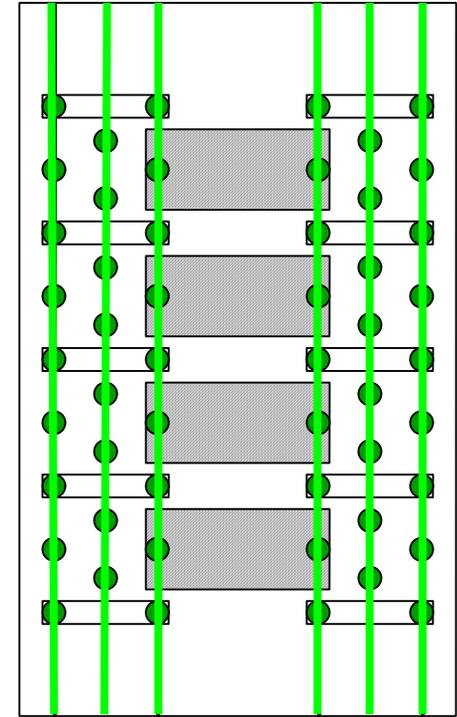
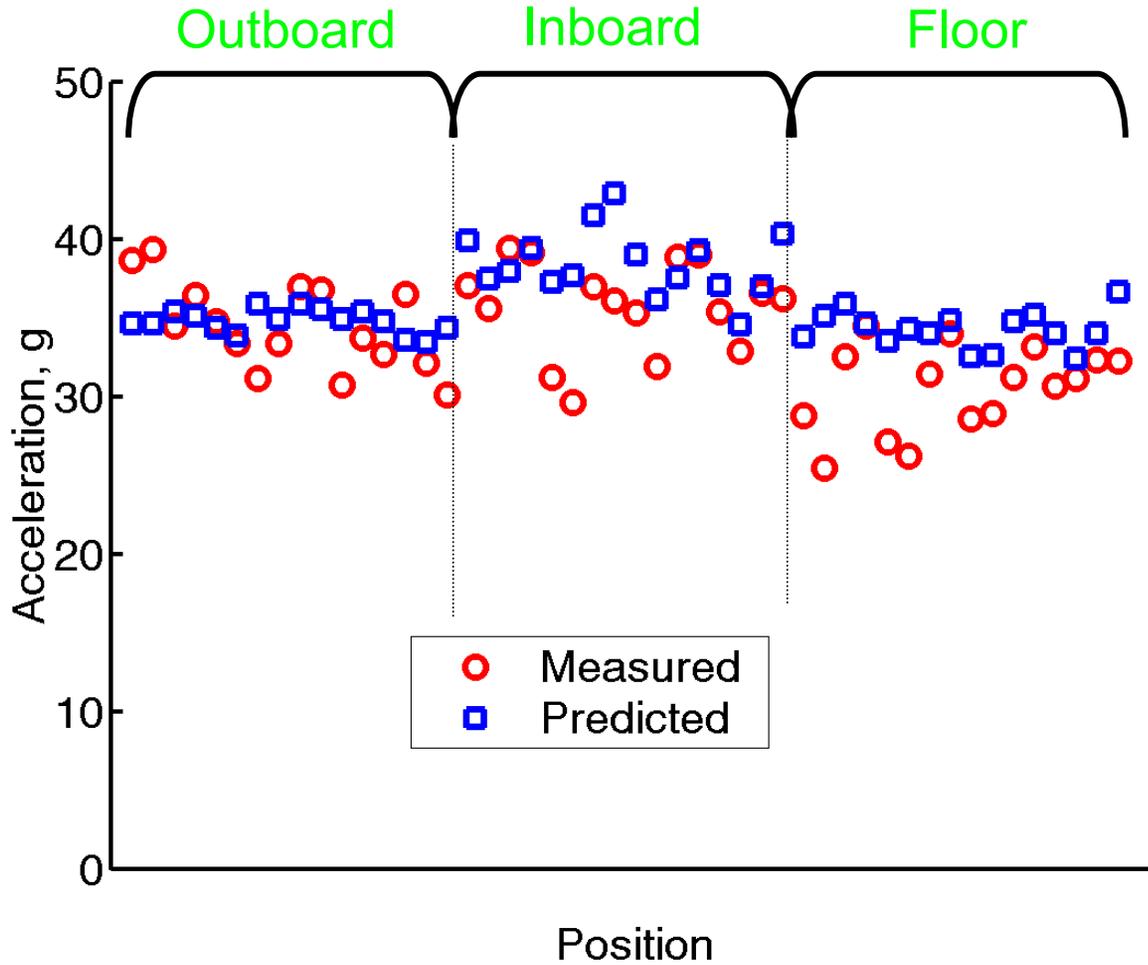
Under-sampled predictions can result in:

- unreliable and inaccurate correlations between measured and predicted
- erroneous modeling modifications



Maximum Accelerations

(Filter Frequency = 100 Hz)

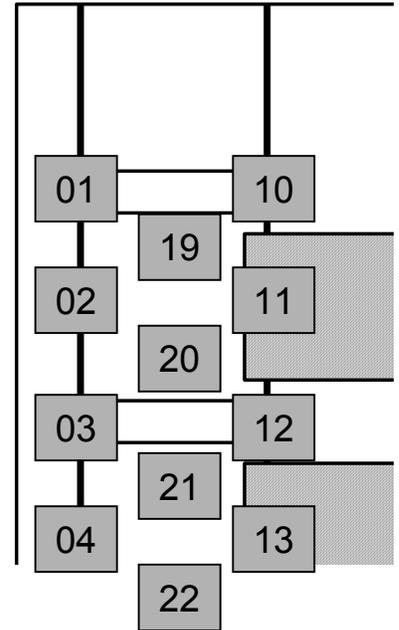
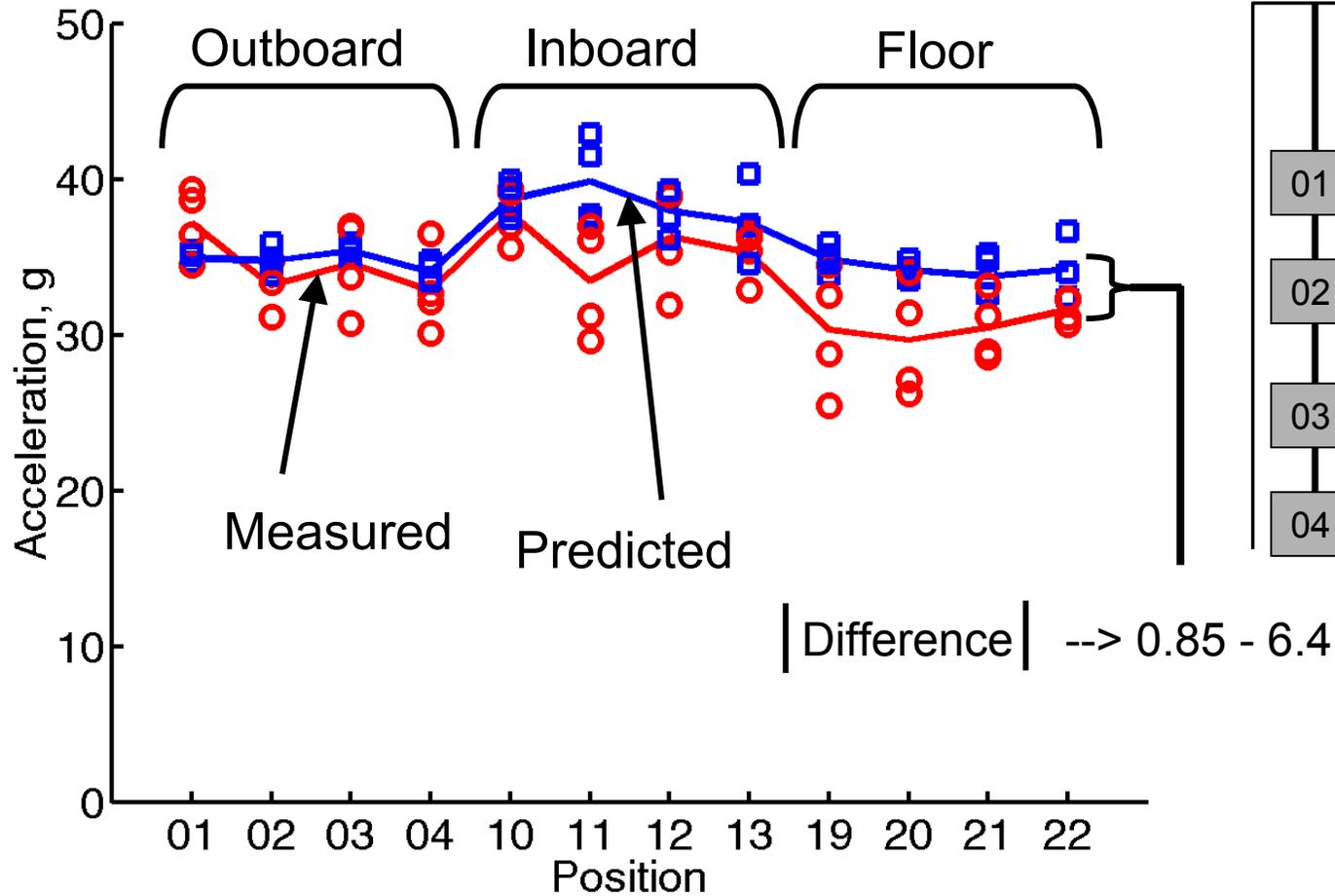


Top View



Maximum Accelerations

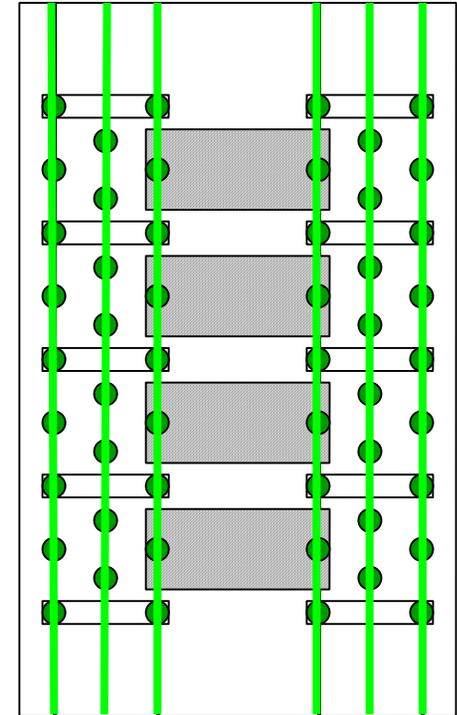
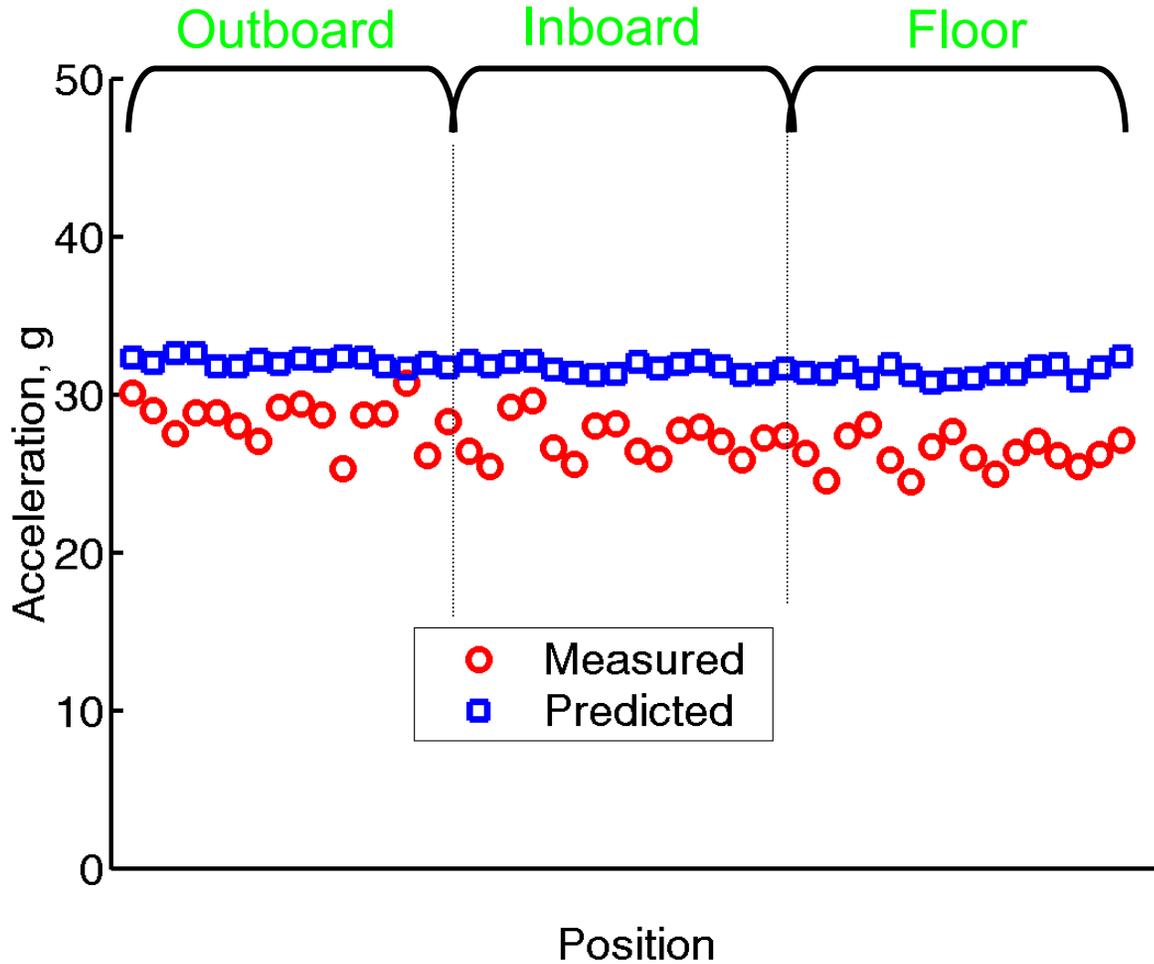
(Filter Frequency = 100 Hz)





Maximum Accelerations

(Filter Frequency = 24 Hz)

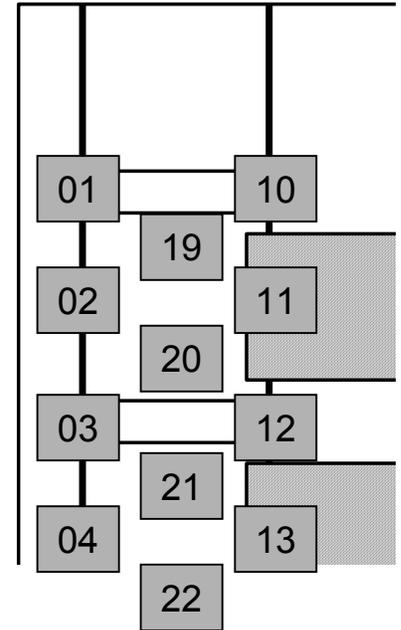
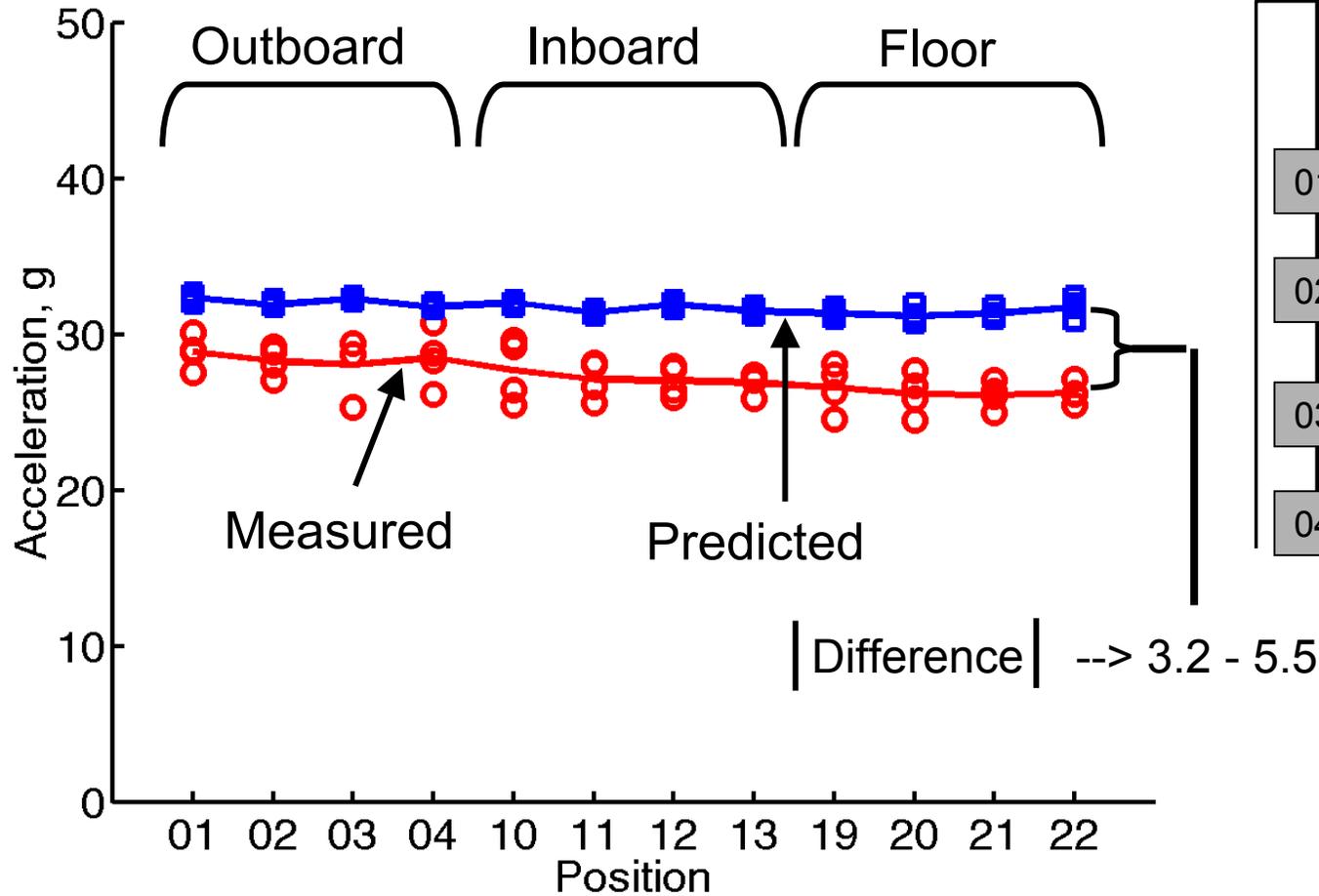


Top View



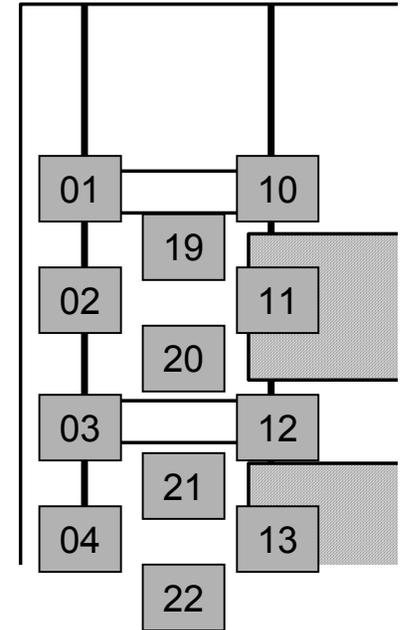
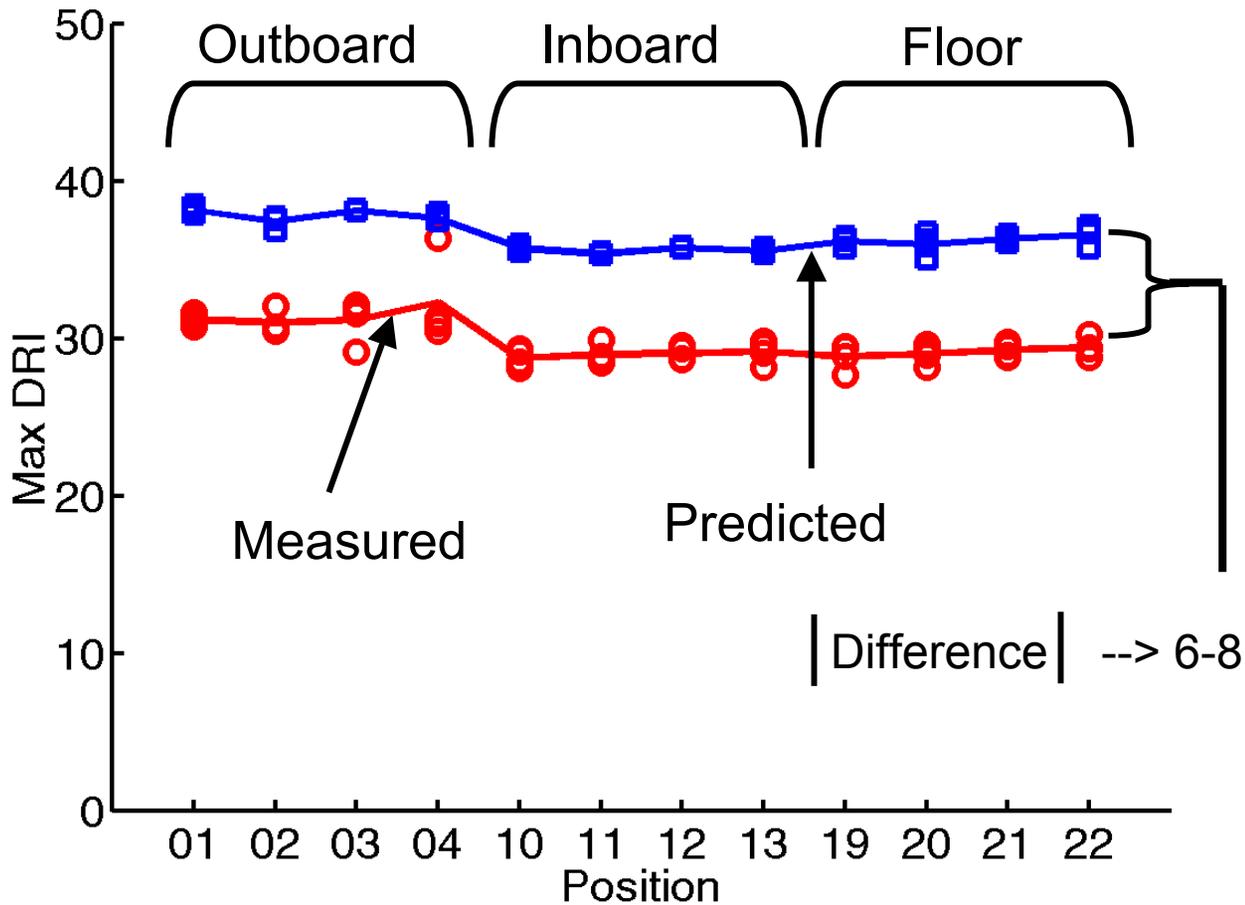
Maximum Accelerations

(Filter Frequency = 24 Hz)





1-D Dynamic Response Index (DRI)*



* DRI computed to evaluate closeness of results.
DO NOT compare with human injury criteria.



Concluding Remarks

- High channel count valuable for identifying similarities and anomalies
- Several correlation methodologies evaluated
- Filtering frequency affects correlation evaluation
- Under-sampling:
 - Readily identified
 - More likely for stiff lightweight structures
 - More prevalent when predicting at measurement points
- Presentation of all locations on one figure:
 - Valuable for global modeling accuracy
 - Highlight subtle and pronounced differences between test and analysis
 - Allow evaluation of several quantities